

## Sensing, Computing, Actuating

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# **CONTROL AND COMPUTATION**

(Chapter 1.5)



**1st phase**

- ▶ Optical and acoustic warning
- ▶ Shock absorber adjustment
- ▶ Precharging of hydraulic brake assist



**2nd phase**

- ▶ Warning jolt
- ▶ Belt slack reduction
- ▶ Partial braking 1 (approx. 30%)



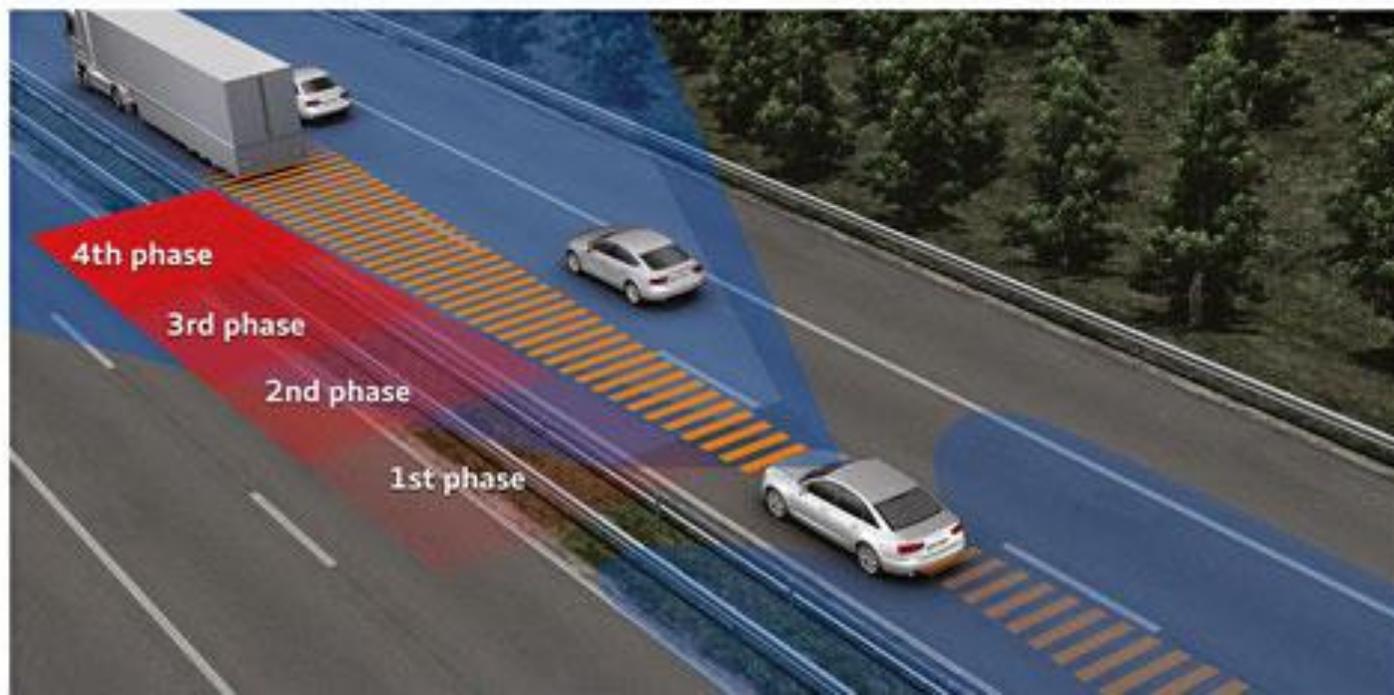
**3rd phase**

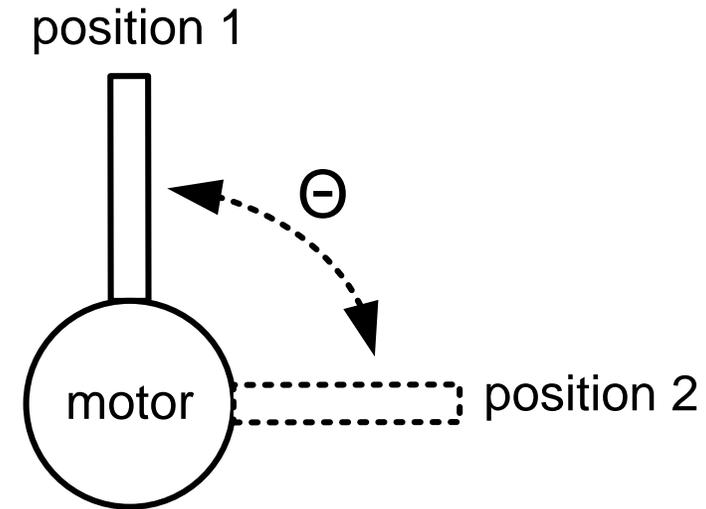
- ▶ Partial braking 2 (approx. 50%)
- ▶ Hazard warning lights
- ▶ Closing of sunroof / windows



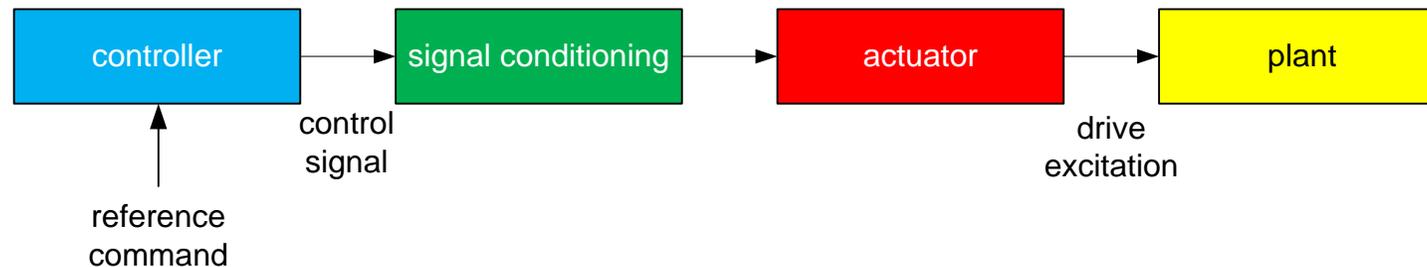
**4th phase**

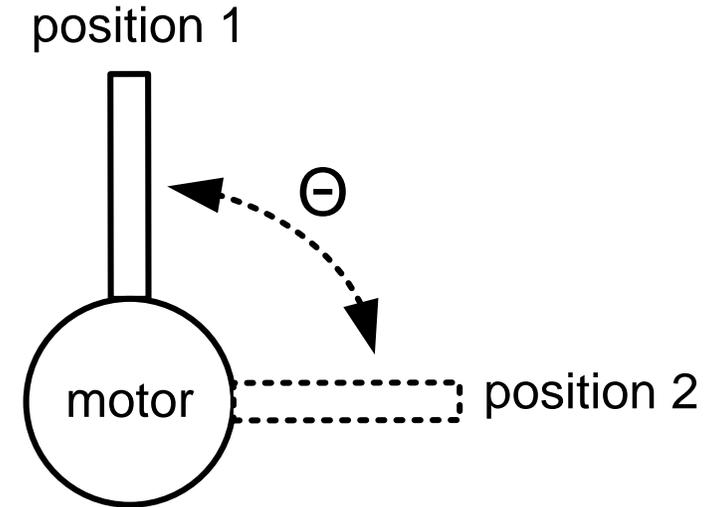
- ▶ Reversible belt tensioner
- ▶ Full brake



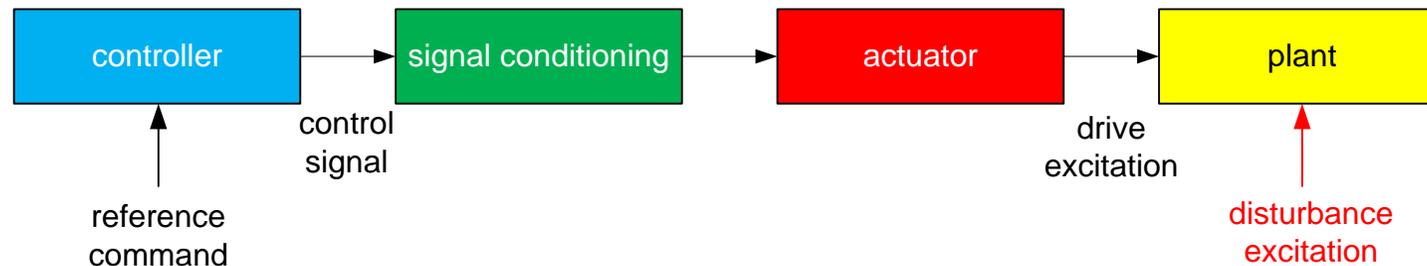


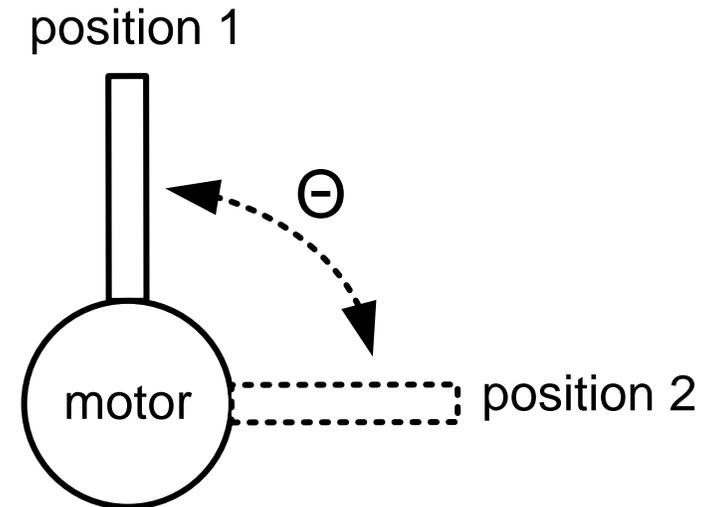
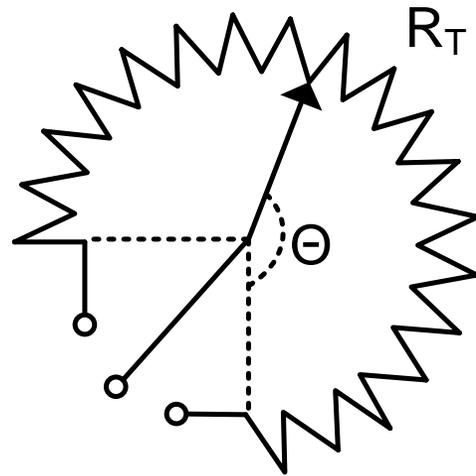
- robot arm needs to travel fixed distance (angle)
- starts at known location, ends at known location
- motor turns with constant speed
- use open-loop controller



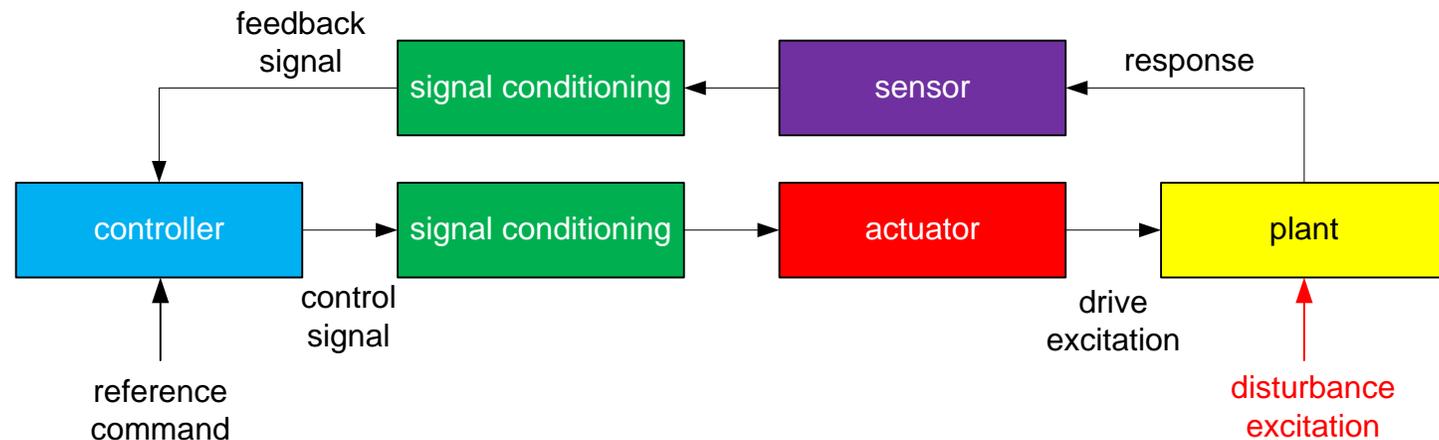


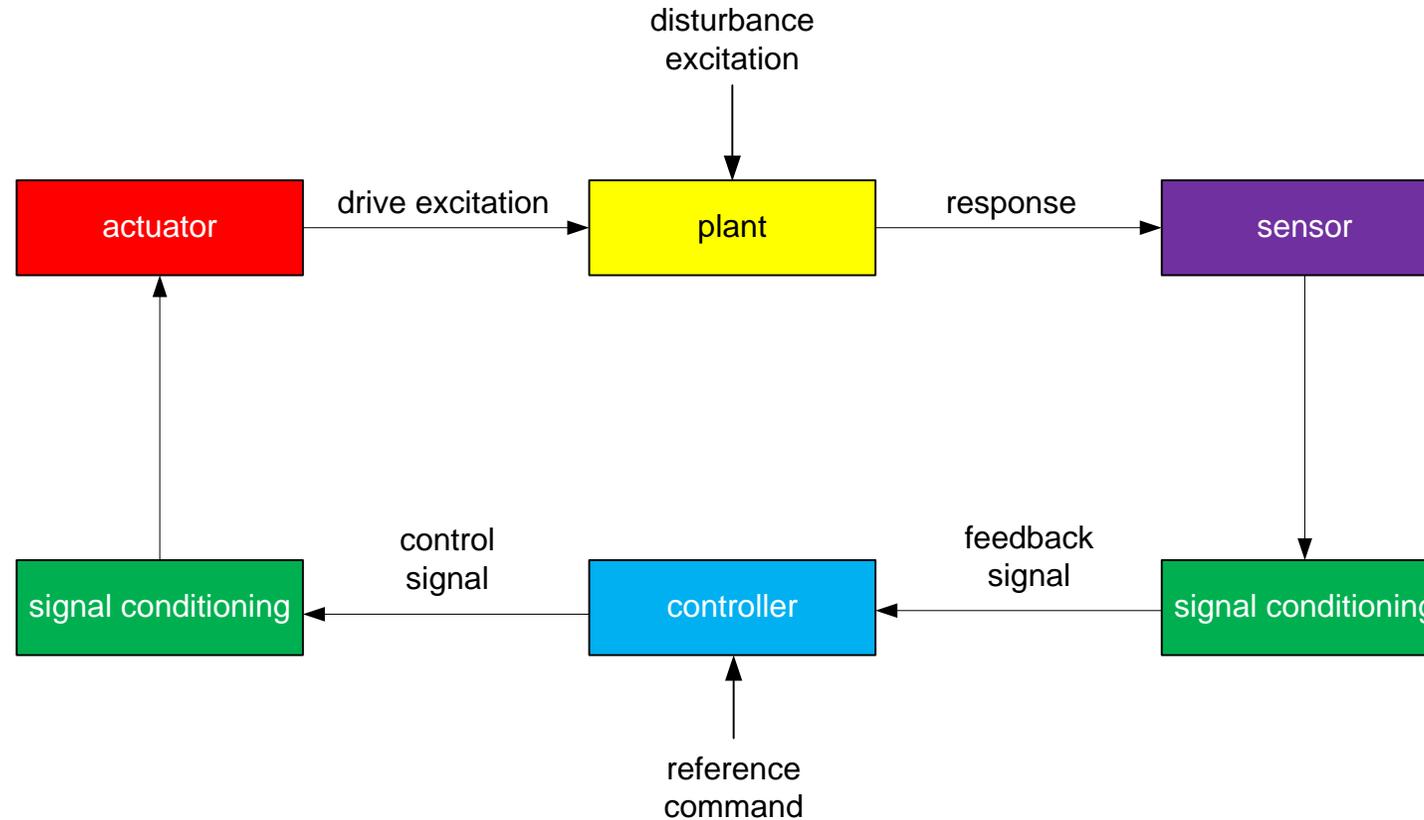
- external disturbances
  - motor speed not constant
  - start, end location not exact
- measure position of arm and use in control system





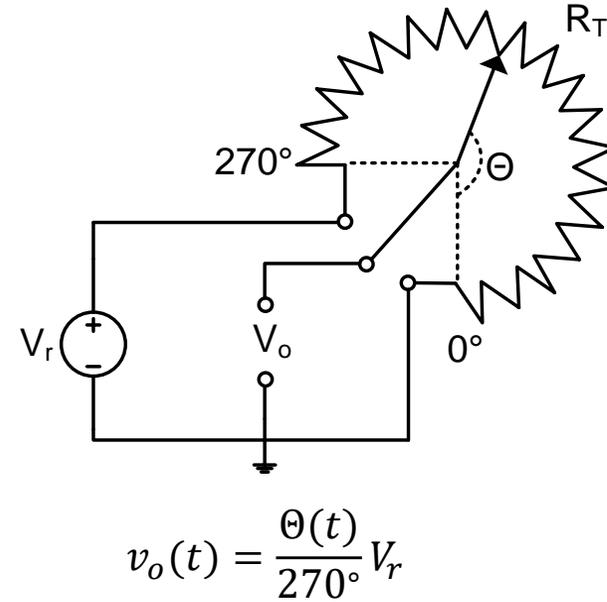
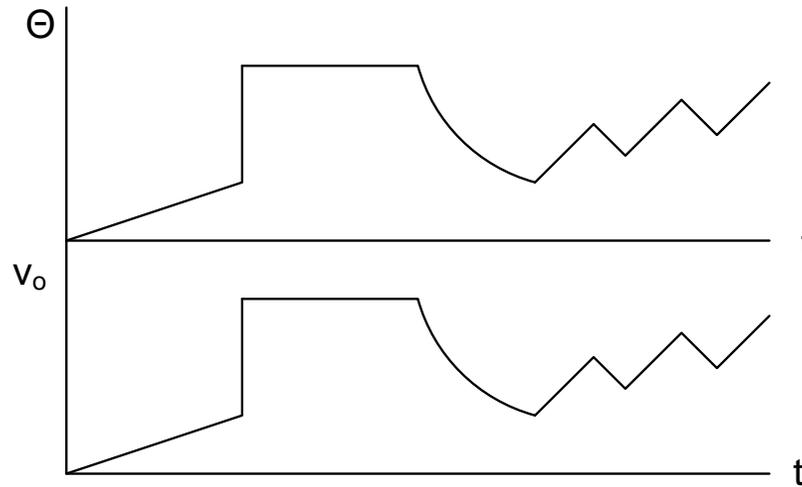
- use potentiometer to measure position
- input: desired angle of arm, output: engine on/off





- measure response and compare with reference to minimize error
- several common feedback control strategies exist
  - on-off control
  - proportional (P) control
  - proportional control with integral (I) and derivative (D) action

- output voltage sensor follows robot arm immediately

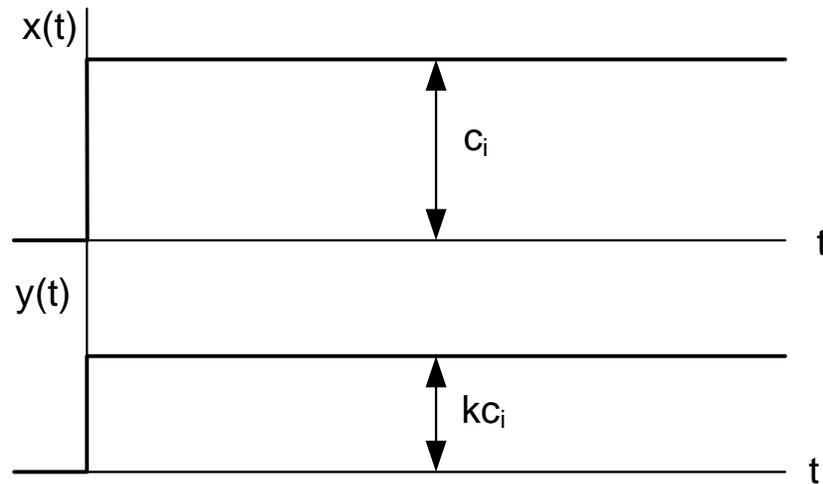


- time-dependent transfer function of robot arm

$$a_0 y(t) = b_0 x(t) \Rightarrow y(t) = \frac{b_0}{a_0} x(t) = k \cdot x(t)$$

- static sensitivity given by  $k$
- system has ideal or perfect dynamic performance

- zero-order system represents ideal or perfect dynamic performance
- demonstrated with response to step at input



step input



frequency response

- no dynamic error present in zero-order systems
- none of the elements in the sensor stores energy



air vent (blower)

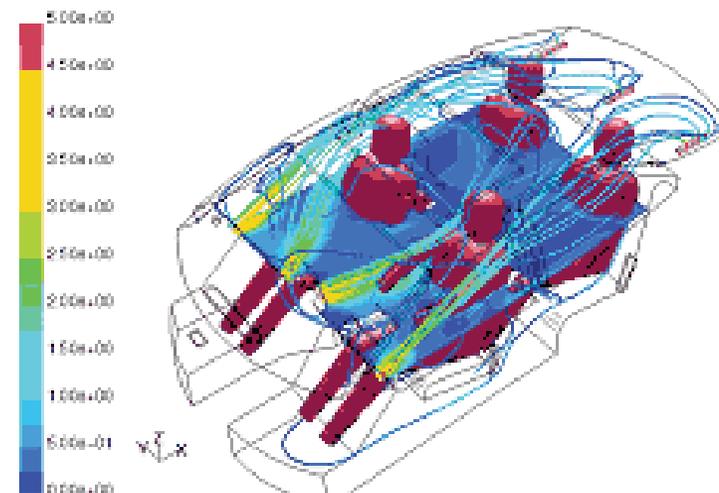
active in-car  
temperaturetemperature  
set point

outside air temperature

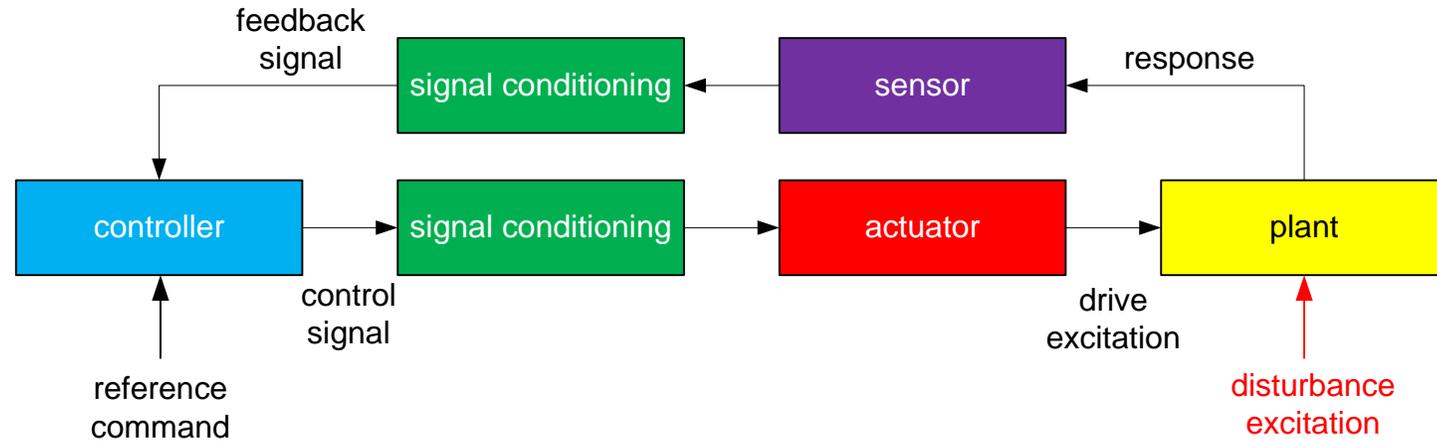
intake air temperature



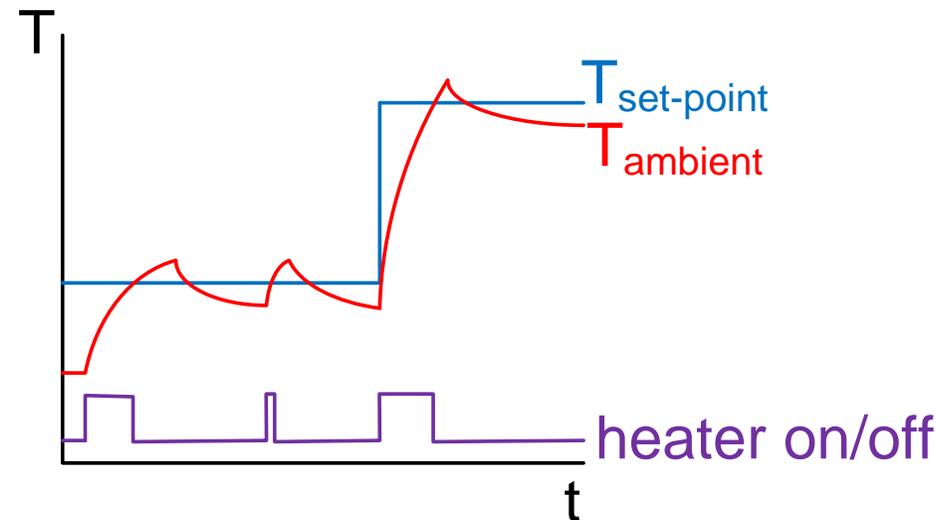
Interior Airflow Pattern



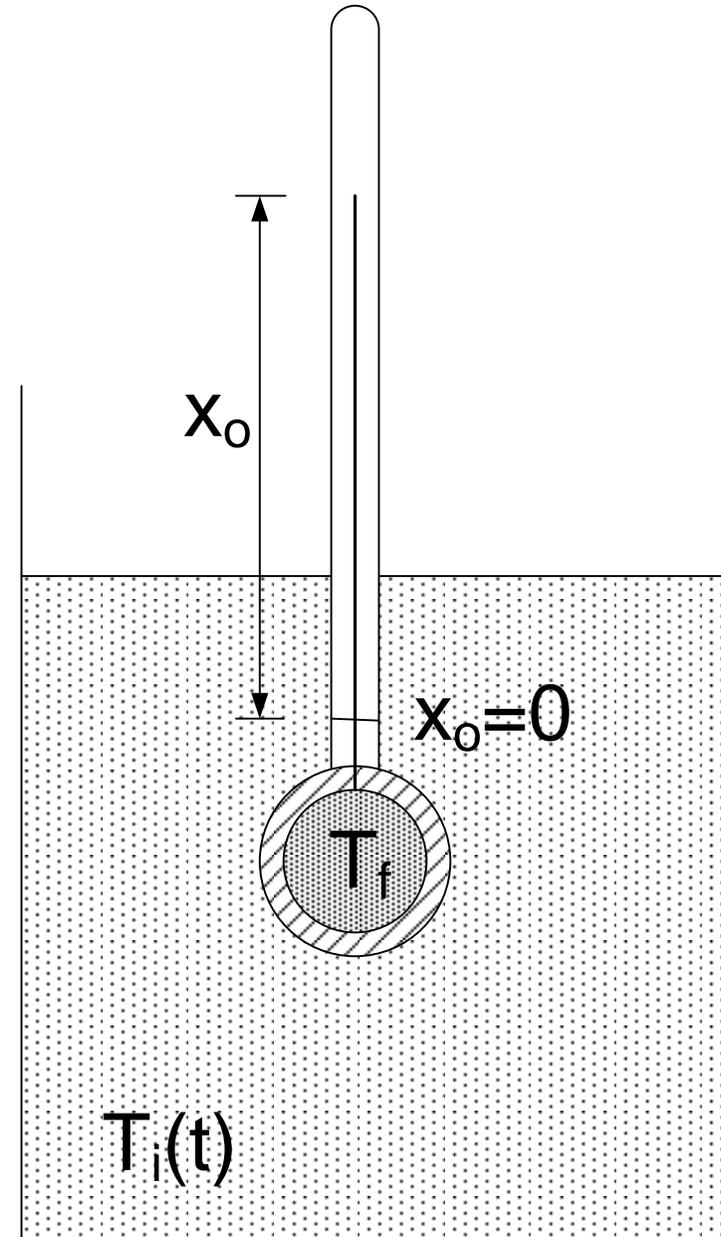
- on/off controller to regulate temperature



- response is not instantaneous
- thermal mass causes delay
- consider time delay in controller



- liquid-in-glass thermometer
  - input – temperature  $T_i(t)$  of environment
  - output – displacement  $x_o$  of the thermometer fluid
  - liquid column has inertia (i.e. transfer function is not ideal)



- first-order system contains one energy storing element
- differential equation for first-order system

$$a_1 \frac{dy(t)}{dt} + a_0 y(t) = b_0 x(t)$$

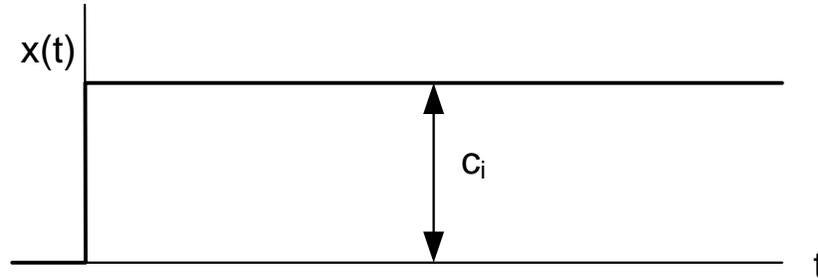
- engineering practice to only consider  $x(t)$  and not its derivatives
- solve equation to obtain transfer function

$$\left. \begin{aligned} \frac{a_1}{a_0} \frac{dy(t)}{dt} + y(t) &= \frac{b_0}{a_0} x(t) \\ k &= \frac{b_0}{a_0}, \quad \tau = \frac{a_1}{a_0} \end{aligned} \right\} \Rightarrow (\tau s + 1)Y(s) = k \cdot X(s) \Rightarrow \frac{Y(s)}{X(s)} = \frac{k}{\tau s + 1}$$

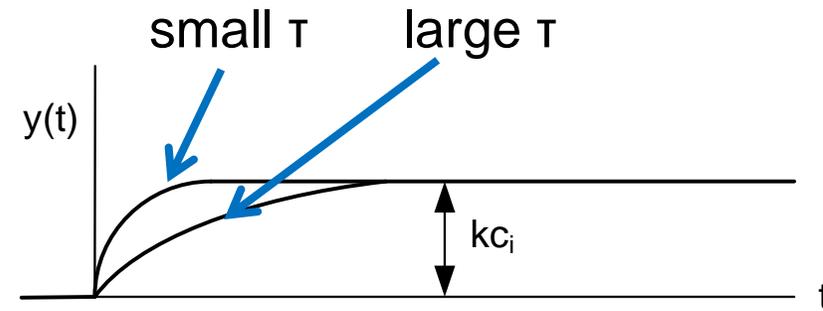
- $k$  – static sensitivity
- $\tau$  – time constant

$$\frac{Y(s)}{X(s)} = \frac{k}{\tau s + 1}, \text{ with } k = \frac{b_0}{a_0}, \tau = \frac{a_1}{a_0}$$

- static input implies all derivatives are zero
- static sensitivity (k) is the amount of output per unit input when the input is static (constant)
- time constant ( $\tau$ ) determines the lag of the output signal on a change in the input signal



step at input



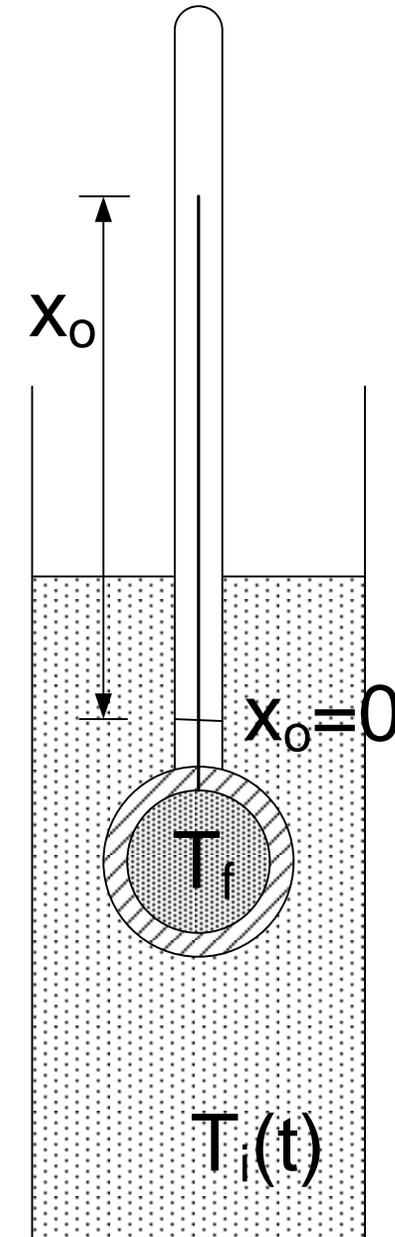
response at output

## Example – liquid-in-glass thermometer

- conservation of energy provides relation between
- fluid temperature ( $T_f$ ) and liquid temperature ( $T_i$ )

$$V_b \rho C \frac{dT_f}{dt} + UA_b T_f = UA_b T_i$$

- $V_b$  – volume of bulb [ $m^3$ ]
- $\rho$  – mass density of thermometer fluid [ $kg/m^3$ ]
- $C$  – specific heat of thermometer fluid [ $J/(kg^\circ C)$ ]
- $U$  – overall heat-transfer coefficient across bulb wall [ $W/(m^2^\circ C)$ ]
- $A_b$  – heat transfer area of bulb wall [ $m^2$ ]



## Example – liquid-in-glass thermometer

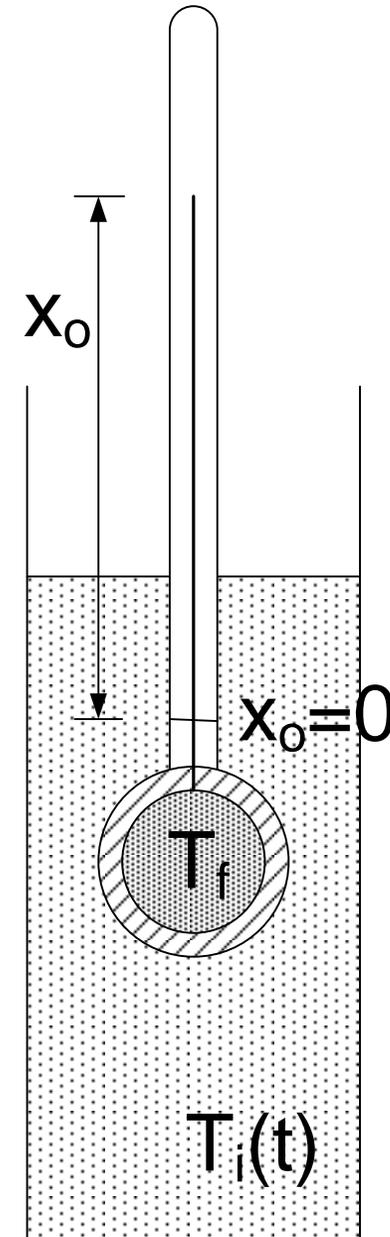
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- fluid temperature ( $T_f$ ) and liquid temperature ( $T_i$ )

$$V_b \rho C \frac{dT_f}{dt} + UA_b T_f = UA_b T_i$$

- relation between liquid level ( $x_o$ ) and fluid temperature ( $T_f$ )

$$x_o = \frac{K_{ex} V_b}{A_c} T_f$$

- $x_o$  – displacement from reference mark [m]
  - $K_{ex}$  – differential expansion coefficient of fluid and bulb [ $m^3/(m^3 \cdot ^\circ C)$ ]
  - $V_b$  – volume of bulb [ $m^3$ ]
  - $A_c$  – cross sectional area of capillary tube [ $m^2$ ]
- what are sensitivity ( $k$ ) and time constant ( $\tau$ )?



## Example – liquid-in-glass thermometer

- conservation of energy provides relation between
- fluid temperature ( $T_f$ ) and liquid temperature ( $T_i$ )

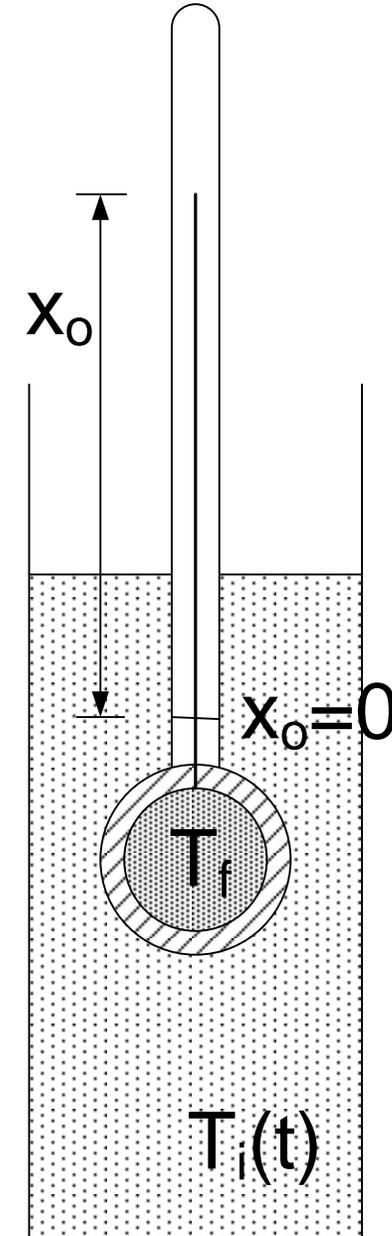
$$V_b \rho C \frac{dT_f}{dt} + UA_b T_f = UA_b T_i$$

- relation between liquid level ( $x_o$ ) and fluid temperature ( $T_f$ )

$$x_o = \frac{K_{ex} V_b}{A_c} T_f$$

- what are sensitivity (k) and time constant ( $\tau$ )?**
- combining equations gives differential equation
- for whole system

$$\left. \begin{aligned}
 V_b \rho C \frac{dT_f}{dt} + UA_b T_f &= UA_b T_i \\
 x_o = \frac{K_{ex} V_b}{A_c} T_f &\Leftrightarrow T_f = \frac{A_c x_o}{K_{ex} V_b}
 \end{aligned} \right\} \Rightarrow \frac{\rho C A_c}{K_{ex}} \frac{dx_o}{dt} + \frac{UA_b A_c}{K_{ex} V_b} x_o = UA_b T_i$$



## Example – liquid-in-glass thermometer

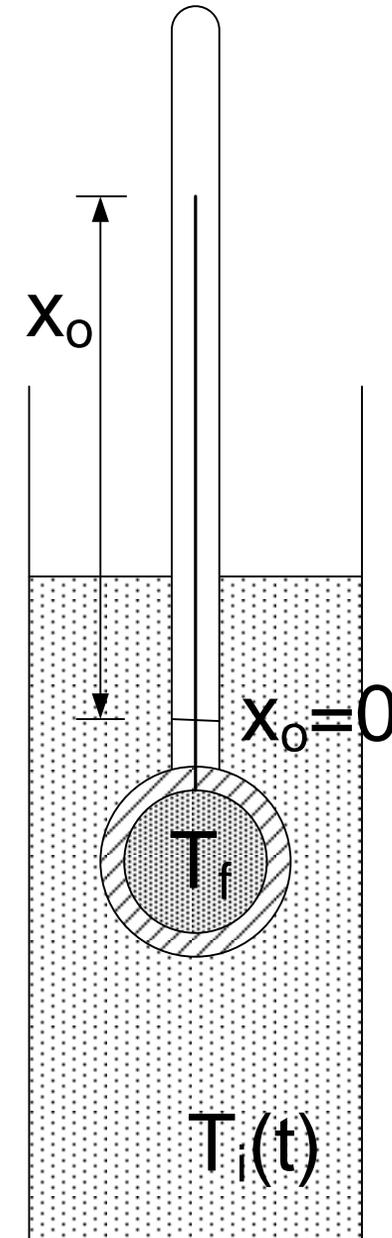
- what are sensitivity ( $k$ ) and time constant ( $\tau$ )?
- combining equations gives differential equation
- for whole system

$$\frac{\rho C A_c}{K_{ex}} \frac{dx_o}{dt} + \frac{U A_b A_c}{K_{ex} V_b} x_o = U A_b T_i$$

- general first-order system

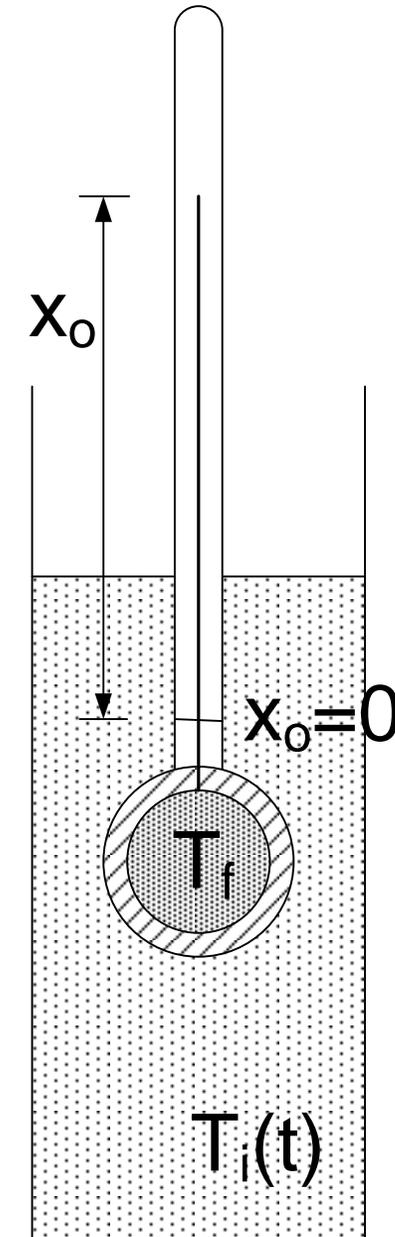
$$\frac{a_1}{a_0} \frac{dy(t)}{dt} + y(t) = \frac{b_0}{a_0} x(t) \Rightarrow k = \frac{b_0}{a_0}, \tau = \frac{a_1}{a_0}$$

- sensitivity [ $\text{m}/^\circ\text{C}$ ]  $k = \frac{K_{ex} V_b}{A_c}$
- time constant [s]  $\tau = \frac{\rho C V_b}{U A_b}$



## Example – liquid-in-glass thermometer

- what are sensitivity ( $k$ ) and time constant ( $\tau$ )?
- sensitivity [ $\text{m}/^\circ\text{C}$ ]  $k = \frac{K_{ex}V_b}{A_c}$
- time constant [ $\text{s}$ ]  $\tau = \frac{\rho CV_b}{UA_b}$
- sensitivity and time constant related to physical parameters
- larger sensitivity ( $k$ ) requires larger bulb volume ( $V_b$ )
- larger bulb volume ( $V_b$ ) increases time constant ( $\tau$ )
- effect partially offset by increased contact area ( $A_b$ )
- careful selection of parameters is required

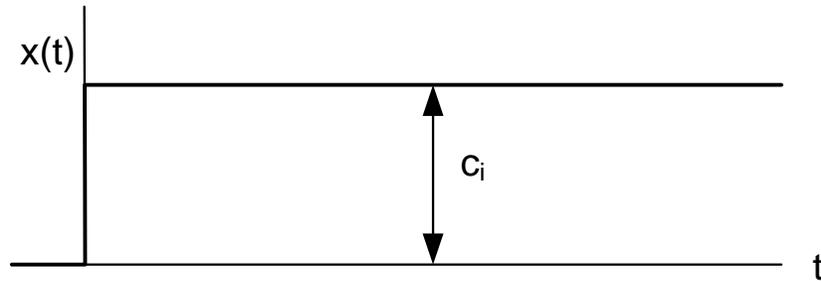


- transfer function is given in Laplace domain

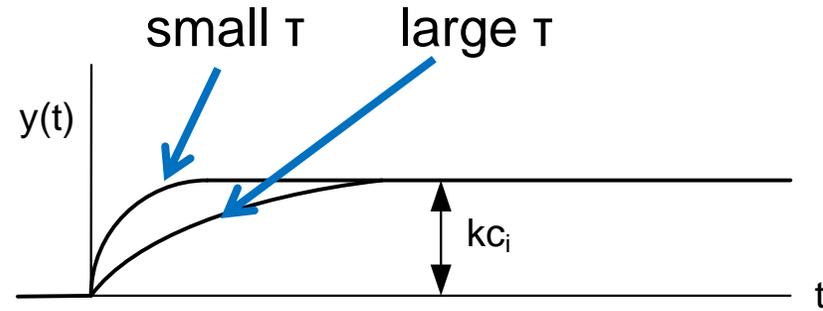
$$\frac{Y(s)}{X(s)} = \frac{k}{\tau s + 1}$$

- what is the response in the time domain to an actual signal?
  - substitute  $X(s)$  with model of input signal
  - apply inverse Laplace transform
- systems usually characterized for some common test inputs
  - step
  - ramp
  - sinusoid
- common test inputs provide insight in behavior of system when real signal is applied

- response to step input ( $c_i=1$ ) is given by  $y(t) = k(1 - e^{-t/\tau})$

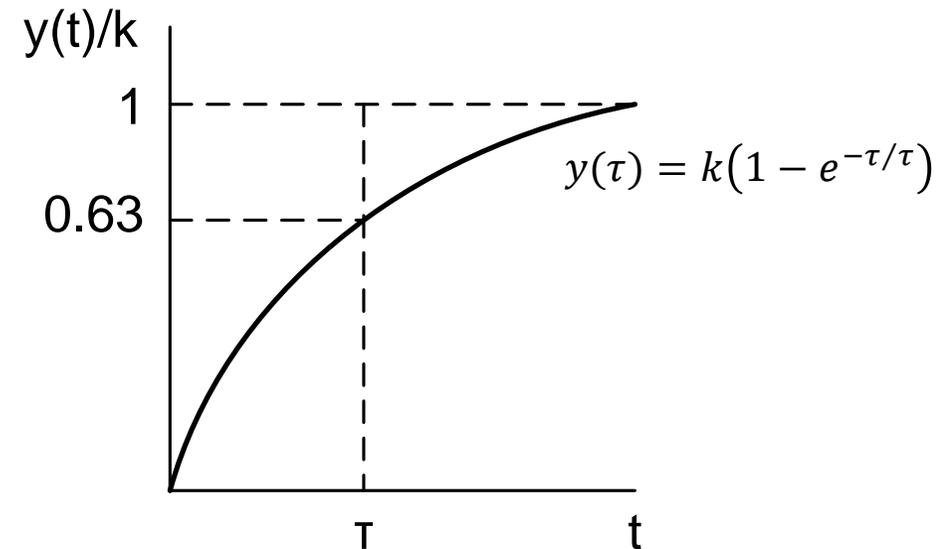


step at input

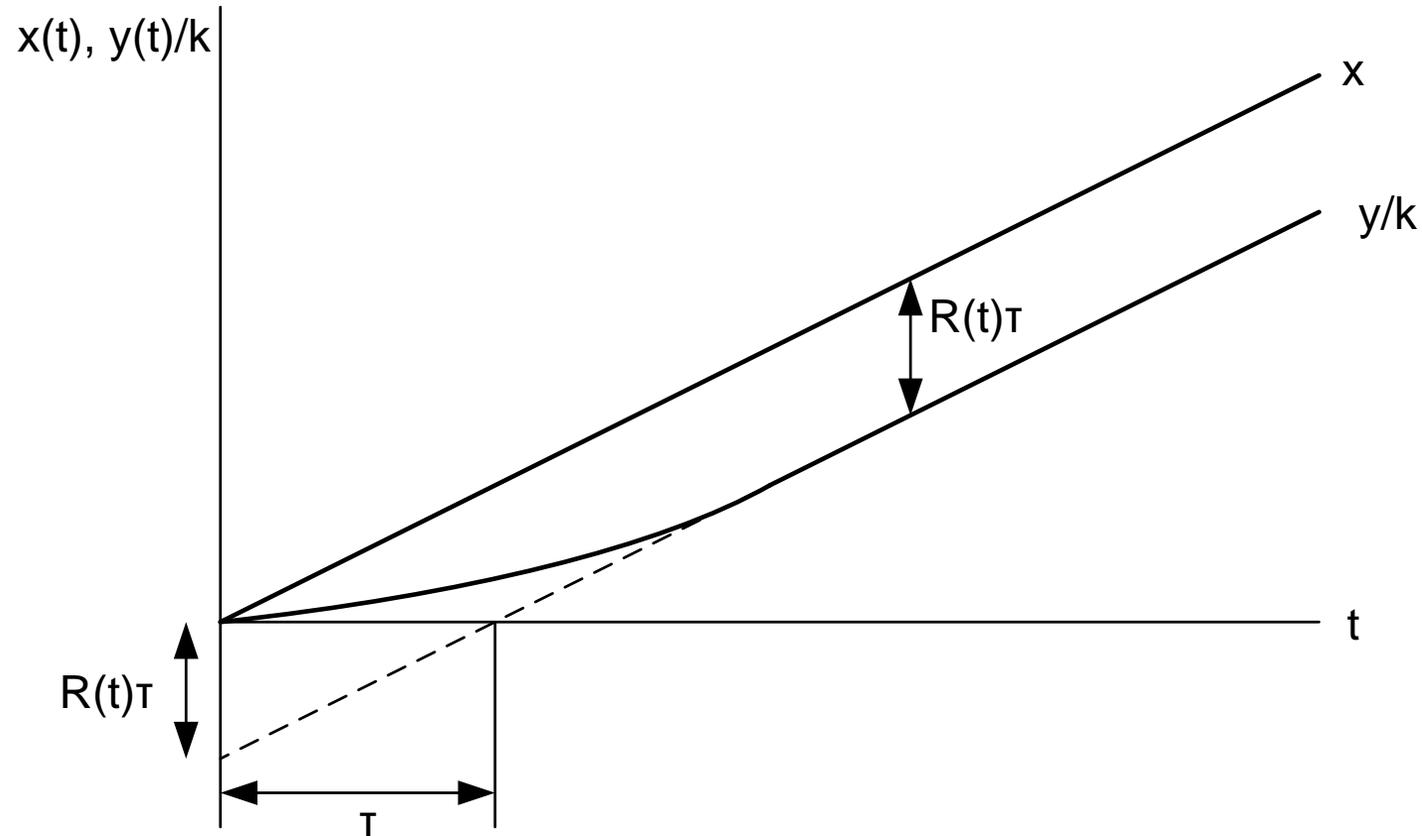


response at output

- two important characteristics
  - dynamic error  $e_d = \lim_{t \rightarrow \infty} y(t) - kx(t)$
  - delay  $t_d = \tau$
- step response has no dynamic error
- step response has a delay



- response to ramp  $R(t)$  input given by  $y(t) = \begin{cases} (1 + \tau e^{-t/\tau})kR(t) & t < 0 \\ (1 + \tau e^{-t/\tau} - \tau)kR(t) & t \geq 0 \end{cases}$



- dynamic error  $e_d = R(t)\tau$
- delay  $t_d = \tau$

- transfer function in Laplace domain

$$\frac{Y(s)}{X(s)} = \frac{k}{\tau s + 1}$$

- response to input  $x(t) = A_i \sin(\omega t)$  given by  $y(t) = A_o \sin(\omega t + \phi)$

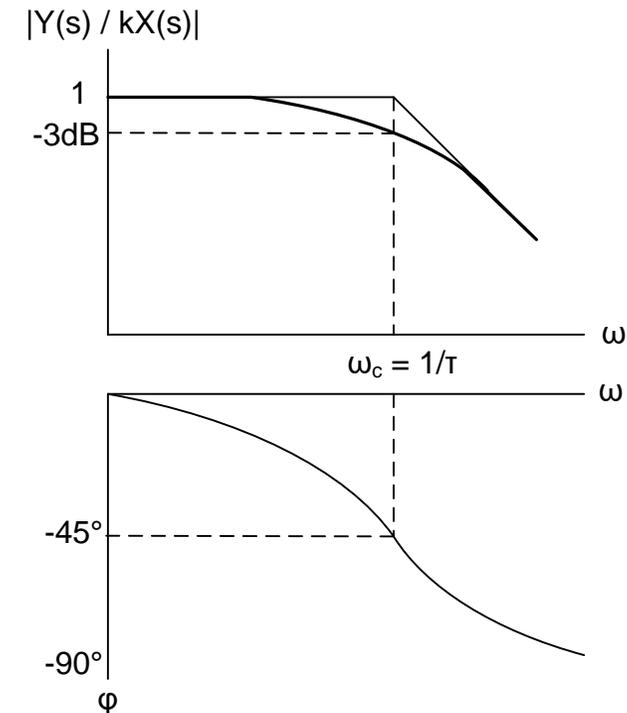
- amplitude ratio  $\frac{A_o}{A_i} = \left| \frac{Y(j\omega)}{X(j\omega)} \right| = \frac{k}{\sqrt{\tau^2 \omega^2 + 1}}$

- phase angle  $\phi = \angle \frac{Y(j\omega)}{X(j\omega)} = \arctan(-\omega\tau)$

- “ideal” (zero-order) sensor has

$$\frac{Y(j\omega)}{X(j\omega)} = k \angle 0^\circ$$

- approached when  $\omega\tau$  is small



- response in time domain is given by

$$\frac{kA_i\tau\omega e^{-t/\tau}}{1 + \omega^2\tau^2} + \frac{kA_i}{\sqrt{1 + \omega^2\tau^2}} \sin(\omega t + \arctan(-\omega\tau))$$

- dynamic error  $e_d = 1 - \frac{1}{\sqrt{1 + \omega^2\tau^2}}$

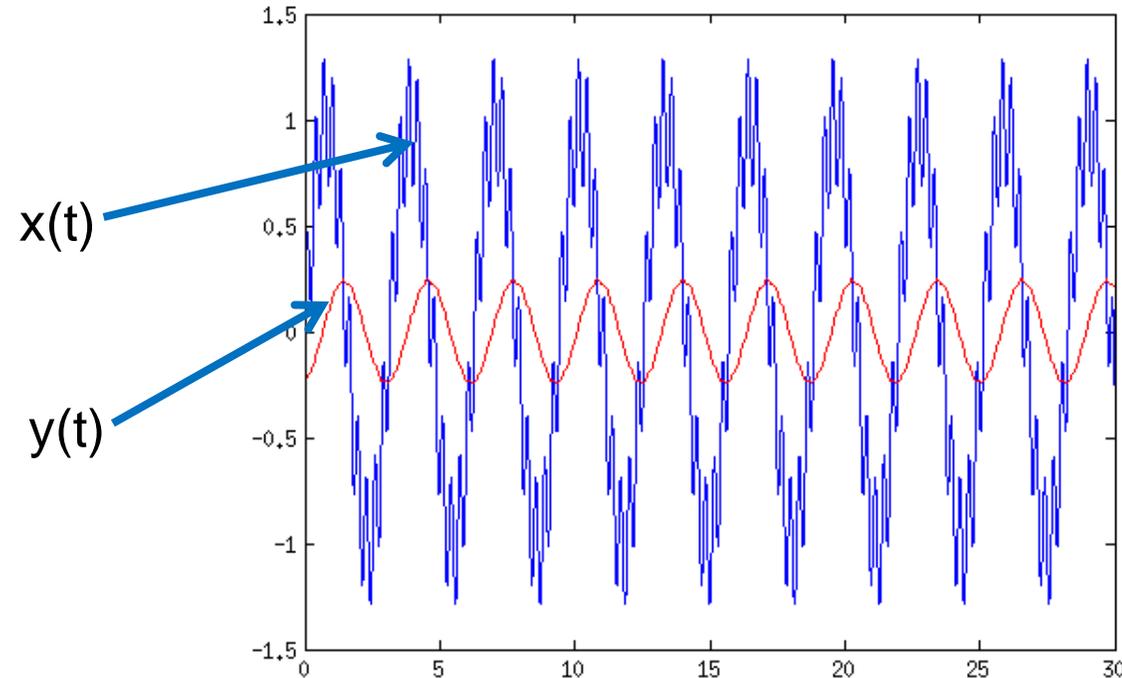
- delay  $t_d = \frac{\arctan(\omega\tau)}{\omega}$

- signal processing can remove
  - amplitude attenuation
  - phase shift
- if the input would be a pure sine wave...
- a more realistic signal may look like
 
$$x(t) = 1 \sin(2t) + 0.3 \sin(20t)$$
- signal is measured with first-order sensor with  $\tau = 2s$ , and static sensitivity  $k$
- **what is  $y(t)$ ?**
- system is linear, therefore use superposition to find  $y(t)$

$$\left. \frac{Y(j\omega)}{X(j\omega)} \right|_{\omega=2} = \frac{k}{\sqrt{\omega^2\tau^2 + 1}} \angle \arctan(-\omega\tau) = \frac{k}{\sqrt{16 + 1}} \angle -76.0^\circ = 0.24k \angle -76.0^\circ$$

$$\left. \frac{Y(j\omega)}{X(j\omega)} \right|_{\omega=20} = \frac{0.3k}{\sqrt{1600 + 1}} \angle -88.6^\circ = 0.007k \angle -88.6^\circ$$

- output equal to  $y(t) = 0.24k \sin(2t - 76.0^\circ) + 0.007k \sin(20t - 88.6^\circ)$



- observations
  - measurement of the input signal is severely distorted (high-frequency component almost invisible)
  - high-frequency component (20 rad/s) is too small compared to low frequency component

- use a different sensor with  $\tau = 0.002s$

$$y(t) = 1.0k \sin(2t - 0.23^\circ) + 0.3k \sin(20t - 2.3^\circ)$$

- comparing output  $y(t)$  to input  $x(t)$

$$x(t) = 1 \sin(2t) + 0.3 \sin(20t)$$

- observation
  - output correctly follows the input
    - amplitude almost equal (except for static sensitivity  $k$ )
    - almost no phase shift
  - selection of correct sensor parameters is very important

## Example – liquid-in-glass thermometer

- time constant  $\tau$  determined by immersing thermometer in a bath; it takes 28s to reach 63% of final reading
- what is the delay when measuring the temperature of a bath that is periodically changing 2 times per minute?**
- time constant  $\tau$  follows from the assignment

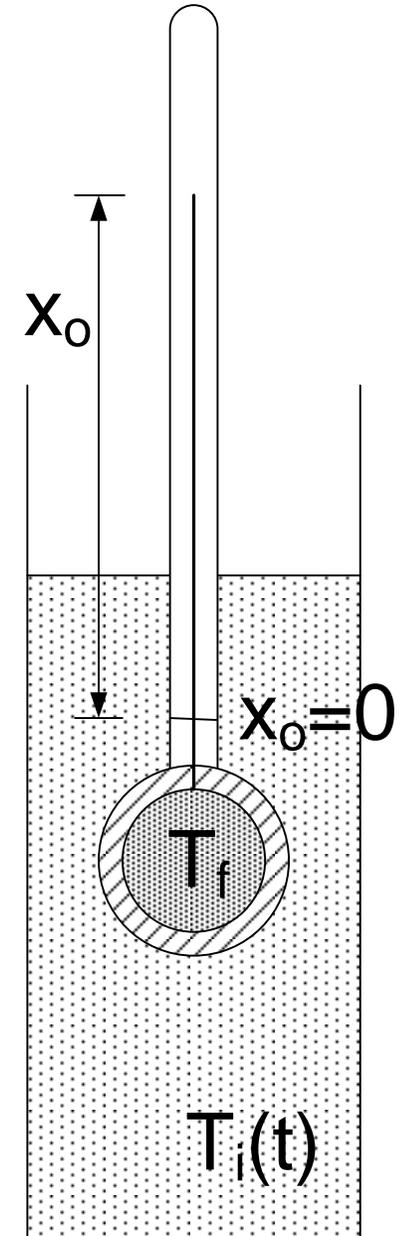
$$\tau = 28s$$

- delay when input varies cyclically is given by

$$t_d = \frac{\arctan(\omega\tau)}{\omega}$$

- angular frequency of temperature to measure

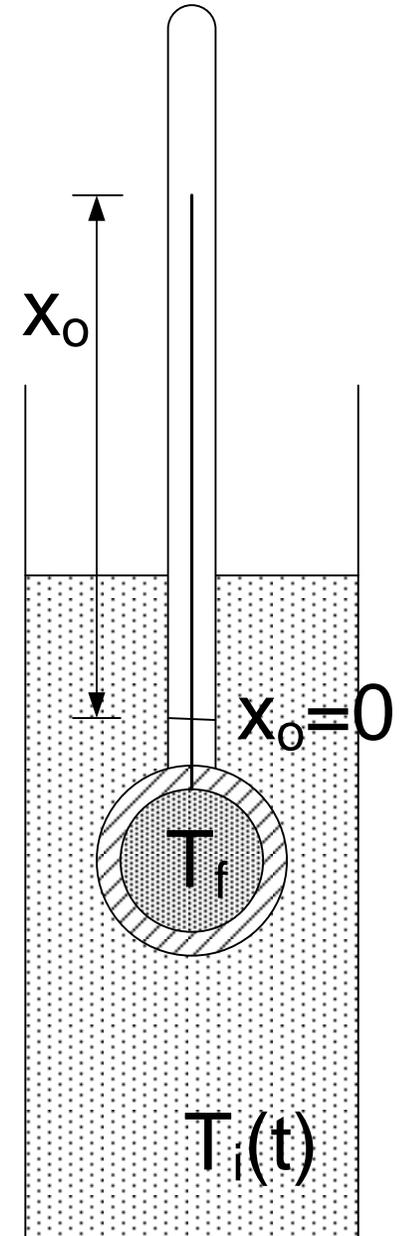
$$\omega = 2\pi \frac{2 \text{ cycles}}{60s} = 0.209 \text{ rad/s}$$



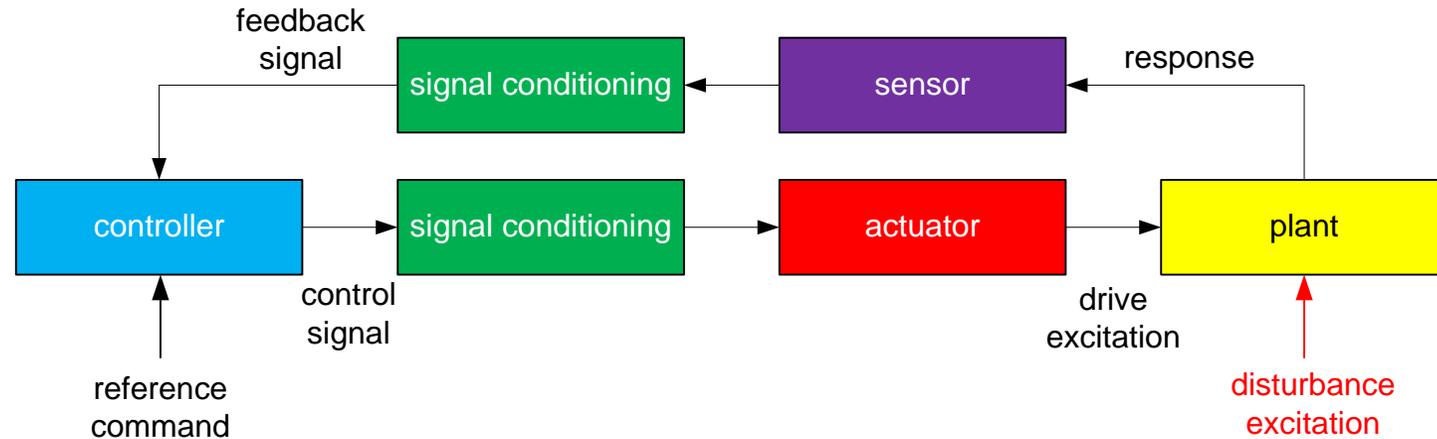
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- time constant  $\tau$  determined by immersing thermometer in a bath; it takes 28s to reach 63% of final reading
- **what is the delay when measuring the temperature of a bath that is periodically changing 2 times per minute?**
- delay is equal to

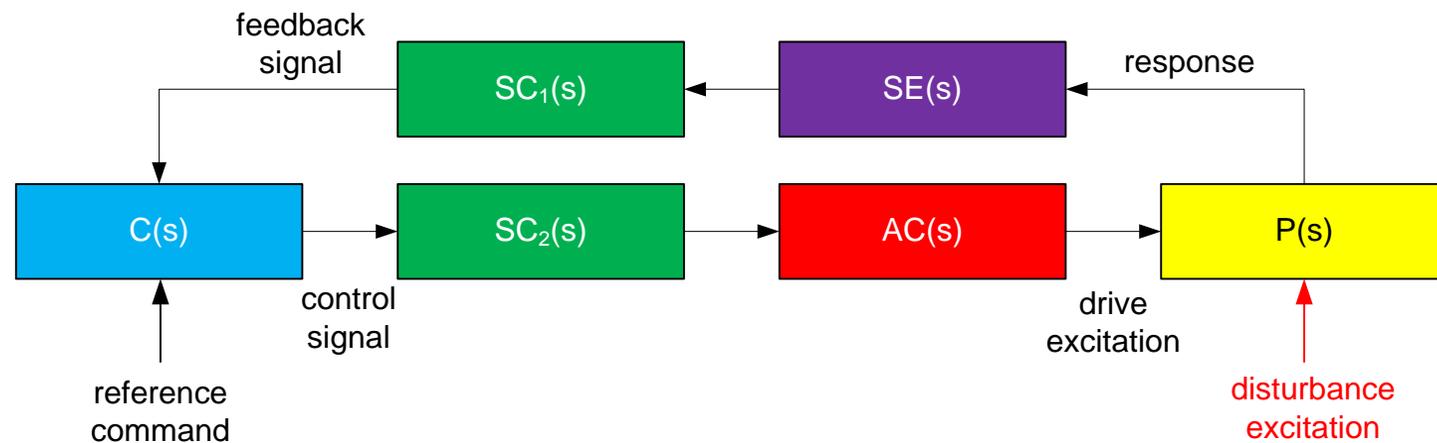
$$t_d = \frac{\arctan\left(\frac{0.209\text{rad}}{1\text{s}} \times 28\text{s}\right)}{0.209\text{rad/s}} = 6.7\text{s}$$



- feedback controller to regulate temperature



- create time-dependent model for each component



- system may consist of many different components each with their own transfer function
- combination of transfer functions of all components gives transfer function of system

